## MEMORANDUM



## 1. Introduction

The purpose of this technical memorandum is to review the traffic impact of a proposed coffee shop to be located at 787 King Street East, Gananoque, Ontario. The site location is shown on Figure 1. A site plan is included in Appendix A.


Figure 1: Site Location

## 2. Existing Conditions

The project site is located on King Street East at Gananoque's eastern gate, in a light commercial area near the Thousand Islands Parkway and Highway 401. The site is currently occupied by a miniature golf course and an information centre. The site driveway is shared with the adjacent Travelodge Motel, 2 residences located behind the motel, and 3 residences located further south on the shore of the St. Lawrence River.

From the project site going west, King Street East is a 3-lane roadway including a 2-way left-turn lane (TWLTL) with a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$. East of the project site, King Street East tapers into a 2-lane roadway. It is identified as Highway 2 between Thousand Islands Parkway and Highway 401, with a posted speed limit of $70 \mathrm{~km} / \mathrm{h}$.

According to MTO's Provincial Highway Traffic Volumes document, Highway 2 has experienced a 1\% growth from 2006 to 2016.

Traffic counts were conducted on King Street East near Carmichael Road by the Town of Gananoque from Friday August 7 to Friday August 14, 2015. The hourly volume for an average weekday (Monday to Thursday) is illustrated in Figure 2.


Figure 2: Average Weekday Hourly Traffic Volume on King Street East, August 2015
The traffic count data indicate that the weekend peak hours were very similar to the average weekday peak hours. Therefore, the average weekday peak hours were used for analysis.

Another traffic count was conducted by BT Engineering on Wednesday April 17, 2019 between 3:00 and 5:30 p.m. near the project site. The traffic volume measured during that period was found to be 1.14 times higher than the traffic volume measured during the same period in August 2015 near Carmichael Road. The
peak hour volumes provided by the Town were therefore multiplied by 1.14 and adjusted using an annual growth rate of $1 \%$ to determine existing (2021) traffic volumes.

The existing traffic volumes near the project site are presented in Table 1.
Table 1: Existing (2021) Traffic Volumes

|  | Morning Peak Hour | Afternoon Peak Hour |
| :--- | :---: | :---: |
| Westbound | 413 | 437 |
| Eastbound | 384 | 621 |

## 3. 2026 Background Traffic

Future background conditions represent the anticipated traffic volumes resulting from general development growth within the region. It is anticipated that the proposed development will be completed in 2021. Therefore, the year 2026 ( 5 years from build-out) has been selected as the planning horizon. An annual growth rate of $1 \%$ has been assumed for analysis.

The 2026 background traffic volumes are presented in Table 2.
Table 2: Background (2026) Traffic Volumes

|  | Morning Peak Hour | Afternoon Peak Hour |
| :--- | :---: | :---: |
| Westbound | 434 | 459 |
| Eastbound | 404 | 653 |

## 4. Trip Generation

The proposed development consists of a Starbucks coffee shop with a drive-through lane. The total floor area is $195 \mathrm{~m}^{2}$ (2,100 sq. ft.).

The Institute of Transportation Engineering's (ITE) Trip Generation Manual 10th Edition is used as a reference to determine the number of trips that will be generated by the development. The "Coffee/Donut Shop with Drive-Through Window" land use (ITE Land Use 937) has been selected to determine the trip generation rates. Table $\mathbf{3}$ presents the number of trips anticipated for the overall development.

As stated above, the project site driveway is shared with the adjacent motel and with 5 houses. The motel can be accessed by 2 other driveways, including one directly in front of it, and each house is expected to generate no more than 1 trip during any peak hour. Therefore, the number of trips using the project site driveway to access either the motel or one of the houses is assumed to be very low. Additionally, many of the trips generated by the coffee shop will come from the adjacent motel as well as the nearby Holiday Inn. These trips will likely be done by foot or using the paved connection between the motel and the proposed
coffee shop. As a result, the number of trips using the coffee shop's driveway will likely be lower than what is calculated in this study and, therefore, the traffic volumes presented below are considered as a worst-case scenario.

Table 3: Trip Generation

| Land Use (ITE Code) | Unit | Item | Morning Peak Hour |  |  | Afternoon Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Total | In | Out | Total | In | Out |
| Coffee/Donut Shop with Drive-Through <br> Window <br> (937) | 1,000 sq. ft. gross floor area | Quantity | 2.7 |  |  | 2.7 |  |  |
|  |  | ITE Trip Rate | 88.99 |  |  | 43.38 |  |  |
|  |  | Pass-By | 60\% |  |  | 60\% |  |  |
|  |  | Distribution | 100\% | 51\% | 49\% | 100\% | 50\% | 50\% |
|  |  | Net Trips | 96 | 49 | 47 | 46 | 23 | 23 |
|  |  | Pass-By Trips | 144 | 72 | 72 | 70 | 35 | 35 |

The proposed development is located in the eastern part of the Town of Gananoque. Part of the net generated trips is expected to come from the town core while the balance is expected to come from Highway 401 or Thousand Islands Parkway. Therefore, it is assumed that $50 \%$ of the net generated trips will be to/from the east and the other $50 \%$ to/from the west.

The proportion of pass-by trips (trips already existing on King Street East) is estimated as 60\% and the distribution is anticipated to be consistent with the current traffic distribution (eastbound/westbound); that is, $48 \%$ eastbound / $52 \%$ westbound during the morning peak hour and $59 \% / 41 \%$ during the afternoon peak hour.

Figure $\mathbf{3}$ presents the trip assignments for the proposed development.


Figure 3: Trip Generation, AM (PM) Peak Hour

## 5. 2026 Total Traffic

The total traffic volumes, reflecting the combined growth in background and site generated traffic, projected for the 2026 planning horizon, are presented in Figure 4.


Figure 4: 2026 Total Traffic Volumes, AM (PM) Peak Hour

A traffic capacity analysis of the projected traffic volumes with the proposed development was performed using the PTV Vistro analysis tool. The methodologies from the Highway Capacity Manual (HCM) were used to determine the volume-to-capacity ( $\mathrm{V} / \mathrm{C}$ ) ratio, average delay per vehicle and 95th percentile queue length for each vehicular movement. The "level of service" (LOS) is directly based on the average delay per vehicle, as described in Table 4. Typically, a LOS D is deemed satisfactory. A LOS E or F may require corrective measures depending on the context.

Table 4: Level of Service Definitions for Unsignalized Intersections

| Delay (s) | LOS |
| :---: | :---: |
| $\leq 10$ | A |
| $\leq 15$ | B |
| $\leq 25$ | C |
| $\leq 35$ | D |
| $\leq 50$ | E |
| $>50$ | F |

The results of the traffic capacity analysis are presented in Table 5. For the purpose of the analysis, nearby driveways were not included as they are not expected to significantly impact the capacity analysis. PTV Vistro reports are provided in Appendix C.

Table 5: Intersection Performance, 2026 Total Traffic

| Intersection | Movement ${ }^{1}$ | Morning Peak Hour |  |  |  | Afternoon Peak Hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { V/C } \\ & \text { Ratio } \end{aligned}$ | Delay <br> (s) |  | 95th <br> Queue (m) | $\begin{aligned} & \text { V/C } \\ & \text { Ratio } \end{aligned}$ | Delay <br> (s) |  | 95th <br> Queue (m) |
| King Street East / | EBT/R | 0.00 | 0 | A | 0 | 0.00 | 0 | A | 0 |
| driveway | WBL/T | 0.05 | 1 | A | 1 | 0.02 | 0 | A | 1 |
| (NB stop) | NBL/R | 0.18 | 18 | C | 8 | 0.11 | 20 | C | 4 |

The overall impact of the proposed development is minor and there are no issues anticipated at the proposed driveways within the 2026 planning horizon.

## 6. Sightline Analysis

A sightline analysis has been completed on the east side of the driveway to determine if the gate structure in front of the project site causes any obstruction.

Two kinds of distance are considered in the sightline analysis: stopping sight distance and intersection sight distance. The stopping sight distance is the distance required for a driver on the roadway to comfortably brake to a halt, including reaction time. The intersection sight distance is the distance required for a driver waiting for a gap (i.e., leaving the parking lot) to determine if the gap in traffic is sufficient to enter the roadway.

Table 6 presents the different sight distances based on design speed, according to TAC's Geometric Design Guide for Canadian Roads. Since the intersection sight distance is longer than the stopping sight distance, the former is used for the sightline analysis.

Table 6: Design Sight Distances

| Design Speed | Stopping Sight <br> Distance $(\mathbf{m})$ | Intersection Sight <br> Distance (m) |
| :---: | :---: | :---: |
| $50 \mathrm{~km} / \mathrm{h}$ | 65 | 105 |
| $60 \mathrm{~km} / \mathrm{h}$ | 85 | 130 |

Assuming a design speed of $60 \mathrm{~km} / \mathrm{h}$, a driver leaving the project site and performing a left turn should be able to see oncoming traffic up to 130 m . The sightline from the project site is shown on Figure 5.


Figure 5: Departure Sightline
As illustrated, the driver exiting the project site will be able to see up to 130 m from their location, and even beyond since the roadway is curved to the north from that point. It is therefore concluded that no sightline issue is anticipated with the presence of the gate.

## 7. Conclusion

The project site is located on King Street East in a light commercial area near Thousand Islands Parkway and Highway 401. The posted speed limit is $50 \mathrm{~km} / \mathrm{h}$ and a 2-way left-turn lane (TWLTL) is provided to facilitate left-turn movements to businesses on each side of the street.

The above analysis determined that no traffic capacity issue is expected to result from the proposed development of a coffee shop and that the gate in front of the project site is not expected to cause any sightline issue with drivers exiting the site. The proposed driveways are expected to operate satisfactorily and, as a result, no roadway improvements to accommodate additional traffic are required.

## Appendix A Site Plan



## Appendix B Traffic Count Data

Roadway
King Street East in Gananoque, ON

|  |  | 7 Aug 2015 | 8 | 9 | 10 | 11 | 12 | 13 | 14 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | End | Fri | Sat | Sun | Mon | Tue | Wed | Thu | Fri |
| 0:00 | 1:00 |  | 71 | 72 | 35 | 38 | 22 | 24 | 39 |
| 1:00 | 2:00 |  | 52 | 38 | 24 | 35 | 32 | 24 | 35 |
| 2:00 | 3:00 |  | 15 | 35 | 16 | 18 | 18 | 27 | 12 |
| 3:00 | 4:00 |  | 24 | 20 | 9 | 5 | 14 | 22 | 24 |
| 4:00 | 5:00 |  | 27 | 12 | 33 | 62 | 36 | 33 | 42 |
| 5:00 | 6:00 |  | 59 | 47 | 71 | 102 | 92 | 92 | 93 |
| 6:00 | 7:00 |  | 125 | 95 | 221 | 191 | 176 | 207 | 222 |
| 7:00 | 8:00 |  | 250 | 170 | 300 | 271 | 285 | 295 | 315 |
| 8:00 | 9:00 | 350 | 284 | 258 | 351 | 323 | 309 | 341 | 364 |
| 9:00 | 10:00 | 373 | 374 | 364 | 364 | 373 | 336 | 380 | 419 |
| 10:00 | 11:00 | 445 | 428 | 383 | 410 | 373 | 386 | 401 | 442 |
| 11:00 | 12:00 | 450 | 451 | 464 | 395 | 364 | 389 | 407 | 459 |
| 12:00 | 13:00 | 456 | 437 | 430 | 420 | 442 | 478 | 477 |  |
| 13:00 | 14:00 | 484 | 470 | 473 | 498 | 438 | 455 | 453 |  |
| 14:00 | 15:00 | 495 | 504 | 507 | 486 | 432 | 467 | 429 |  |
| 15:00 | 16:00 | 535 | 498 | 492 | 562 | 503 | 557 | 534 |  |
| 16:00 | 17:00 | 527 | 512 | 505 | 531 | 511 | 535 | 563 |  |
| 17:00 | 18:00 | 544 | 495 | 420 | 516 | 479 | 538 | 521 |  |
| 18:00 | 19:00 | 448 | 412 | 374 | 474 | 437 | 406 | 452 |  |
| 19:00 | 20:00 | 349 | 352 | 346 | 352 | 322 | 351 | 370 |  |
| 20:00 | 21:00 | 330 | 291 | 293 | 321 | 295 | 308 | 380 |  |
| 21:00 | 22:00 | 346 | 219 | 239 | 194 | 214 | 208 | 304 |  |
| 22:00 | 23:00 | 224 | 281 | 136 | 135 | 204 | 218 | 233 |  |
| 23:00 | 0:00 | 157 | 98 | 99 | 108 | 95 | 96 | 117 |  |



Roadway
King Street East in Gananoque, ON

|  |  | 7 Aug 2015 | 8 | 9 | 10 | 11 | 12 | 13 | 14 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | End | Fri | Sat | Sun | Mon | Tue | Wed | Thu | Fr |
| 0:00 | 1:00 |  | 87 | 70 | 38 | 36 | 35 | 29 | 39 |
| 1:00 | 2:00 |  | 55 | 52 | 26 | 17 | 32 | 25 | 24 |
| 2:00 | 3:00 |  | 35 | 26 | 24 | 26 | 26 | 24 | 20 |
| 3:00 | 4:00 |  | 27 | 19 | 12 | 10 | 15 | 32 | 22 |
| 4:00 | 5:00 |  | 34 | 23 | 34 | 38 | 32 | 39 | 40 |
| 5:00 | 6:00 |  | 51 | 34 | 58 | 76 | 69 | 63 | 73 |
| 6:00 | 7:00 |  | 118 | 94 | 277 | 246 | 253 | 268 | 278 |
| 7:00 | 8:00 |  | 261 | 160 | 357 | 302 | 340 | 355 | 377 |
| 8:00 | 9:00 | 434 | 366 | 265 | 403 | 392 | 396 | 429 | 387 |
| 9:00 | 10:00 | 451 | 479 | 396 | 430 | 399 | 400 | 416 | 441 |
| 10:00 | 11:00 | 459 | 454 | 436 | 449 | 414 | 409 | 402 | 477 |
| 11:00 | 12:00 | 472 | 515 | 479 | 443 | 419 | 465 | 448 | 472 |
| 12:00 | 13:00 | 523 | 500 | 453 | 453 | 461 | 473 | 474 |  |
| 13:00 | 14:00 | 488 | 440 | 474 | 438 | 464 | 466 | 422 |  |
| 14:00 | 15:00 | 507 | 491 | 482 | 464 | 449 | 454 | 464 |  |
| 15:00 | 16:00 | 475 | 423 | 440 | 395 | 417 | 448 | 414 |  |
| 16:00 | 17:00 | 437 | 493 | 422 | 398 | 414 | 427 | 473 |  |
| 17:00 | 18:00 | 481 | 412 | 384 | 397 | 409 | 405 | 452 |  |
| 18:00 | 19:00 | 441 | 379 | 363 | 319 | 376 | 411 | 394 |  |
| 19:00 | 20:00 | 414 | 355 | 335 | 316 | 302 | 334 | 370 |  |
| 20:00 | 21:00 | 332 | 289 | 286 | 243 | 253 | 254 | 306 |  |
| 21:00 | 22:00 | 295 | 235 | 231 | 167 | 199 | 171 | 213 |  |
| 22:00 | 23:00 | 177 | 198 | 158 | 135 | 158 | 174 | 195 |  |
| 23:00 | 0:00 | 141 | 121 | 119 | 84 | 71 | 57 | 85 |  |



## Appendix C PTV Vistro Analysis

Control Type: Analysis Method: Analysis Period:

Two-way stop HCM 6th Edition 15 minutes

Delay (sec / veh):
Level Of Service:
Volume to Capacity ( $\mathrm{v} / \mathrm{c}$ ):
21.5

C
0.180

Intersection Setup

| Name | proposed development |  | King St E |  | King St E |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  | Eastbound |  | Westbound |  |
| Lane Configuration | $T$ |  | $\stackrel{F}{F}$ |  | $4$ |  |
| Turning Movement | Left | Right | Thru | Right | Left | Thru |
| Lane Width [m] | 3.50 | 3.50 | 3.50 | 3.50 | 3.50 | 3.50 |
| No. of Lanes in Entry Pocket | 0 | 0 | 0 | 0 | 0 | 0 |
| Entry Pocket Length [m] | 30.48 | 30.48 | 30.48 | 30.48 | 30.48 | 30.48 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [m] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [km/h] | 50.00 |  | 50.00 |  | 50.00 |  |
| Grade [\%] | 0.00 |  | 0.00 |  | 0.00 |  |
| Crosswalk | No |  | No |  | No |  |

## Volumes

| Name | proposed development |  | King St E |  | King St E |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 47 | 45 | 377 | 46 | 48 | 405 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 47 | 45 | 377 | 46 | 48 | 405 |
| Peak Hour Factor | 0.9500 | 0.9500 | 0.9500 | 0.9500 | 0.9500 | 0.9500 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 12 | 12 | 99 | 12 | 13 | 107 |
| Total Analysis Volume [veh/h] | 49 | 47 | 397 | 48 | 51 | 426 |
| Pedestrian Volume [ped/h] |  | 0 |  | 0 |  |  |

Version 2021 (SP 0-2)
Intersection Settings

| Priority Scheme | Stop | Free |  |
| :---: | :---: | :---: | :---: |
| Flared Lane | No |  |  |
| Storage Area [veh] | 0 | 0 |  |
| Two-Stage Gap Acceptance | No | 0 |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.18 | 0.07 | 0.00 | 0.00 | 0.05 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/veh] | 21.48 | 13.92 | 0.00 | 0.00 | 8.38 | 0.00 |
| Movement LOS | C | B | A | A | A | A |
| 95th-Percentile Queue Length [veh/ln] | 1.00 | 1.00 | 0.00 | 0.00 | 0.14 | 0.14 |
| 95th-Percentile Queue Length [m/ln] | 7.59 | 7.59 | 0.00 | 0.00 | 1.09 | 1.09 |
| d_A, Approach Delay [s/veh] | 17.78 |  | 0.00 |  | 0.90 |  |
| Approach LOS | C |  | A |  | A |  |
| d_I, Intersection Delay [s/veh] | 2.10 |  |  |  |  |  |
| Intersection LOS | C |  |  |  |  |  |


|  | Intersection Level Of Service Report <br> Intersection 1: Project Site Driveway |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Control Type: | Two-way stop | Delay (sec/veh): |  |  |
| Analysis Method: | HCM 6th Edition | Level Of Service: | 26.2 |  |
| Analysis Period: | 15 minutes | Volume to Capacity $(\mathrm{v} / \mathrm{c}):$ | D |  |
|  |  |  | 0.109 |  |

Intersection Setup

| Name | proposed development |  | King St E |  | King St E |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  | Eastbound |  | Westbound |  |
| Lane Configuration | $T$ |  | $\stackrel{F}{F}$ |  | $4$ |  |
| Turning Movement | Left | Right | Thru | Right | Left | Thru |
| Lane Width [m] | 3.50 | 3.50 | 3.50 | 3.50 | 3.50 | 3.50 |
| No. of Lanes in Entry Pocket | 0 | 0 | 0 | 0 | 0 | 0 |
| Entry Pocket Length [m] | 30.48 | 30.48 | 30.48 | 30.48 | 30.48 | 30.48 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [m] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [km/h] | 50.00 |  | 50.00 |  | 50.00 |  |
| Grade [\%] | 0.00 |  | 0.00 |  | 0.00 |  |
| Crosswalk | No |  | No |  | No |  |

## Volumes

| Name | proposed development |  | King St E |  | King St E |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 20 | 25 | 637 | 25 | 20 | 468 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 20 | 25 | 637 | 25 | 20 | 468 |
| Peak Hour Factor | 0.9500 | 0.9500 | 0.9500 | 0.9500 | 0.9500 | 0.9500 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 5 | 7 | 168 | 7 | 5 | 123 |
| Total Analysis Volume [veh/h] | 21 | 26 | 671 | 26 | 21 | 493 |
| Pedestrian Volume [ped/h] |  |  |  | 0 |  | 0 |

Version 2021 (SP 0-2)
Intersection Settings

| Priority Scheme | Stop | Free |  |
| :---: | :---: | :---: | :---: |
| Flared Lane | No |  |  |
| Storage Area [veh] | 0 | 0 |  |
| Two-Stage Gap Acceptance | No | 0 |  |
| Number of Storage Spaces in Median | 0 | 0 | 0 |

Movement, Approach, \& Intersection Results

| V/C, Movement V/C Ratio | 0.11 | 0.06 | 0.01 | 0.00 | 0.02 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d_M, Delay for Movement [s/veh] | 26.22 | 15.57 | 0.00 | 0.00 | 9.10 | 0.00 |
| Movement LOS | D | C | A | A | A | A |
| 95th-Percentile Queue Length [veh/ln] | 0.59 | 0.59 | 0.00 | 0.00 | 0.07 | 0.07 |
| 95th-Percentile Queue Length [m/ln] | 4.49 | 4.49 | 0.00 | 0.00 | 0.55 | 0.55 |
| d_A, Approach Delay [s/veh] | 20.33 |  | 0.00 |  | 0.37 |  |
| Approach LOS | C |  | A |  | A |  |
| d_I, Intersection Delay [s/veh] | 0.91 |  |  |  |  |  |
| Intersection LOS | D |  |  |  |  |  |

